

Resonant Circuit Generates a High-Frequency Magnetic Field

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[KC Yang](#)

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This novel LC resonant tank amplifies the magnetic coil current by 2X while generating a high-frequency magnetic field.

Generating a high-frequency magnetic field can be quite a challenge due to an assortment of technical issues. At high frequency, magnetic-coil impedance is large. It requires a high-voltage and high-frequency generator to produce enough current through the magnetic coil. However, it's difficult to generate high frequency and high current at the same time using conventional amplifiers and drivers. Classic series resonant techniques have been used for high-frequency magnetic-field generation.¹ The resonant circuit proposed in this article will further boost coil current by 2X.

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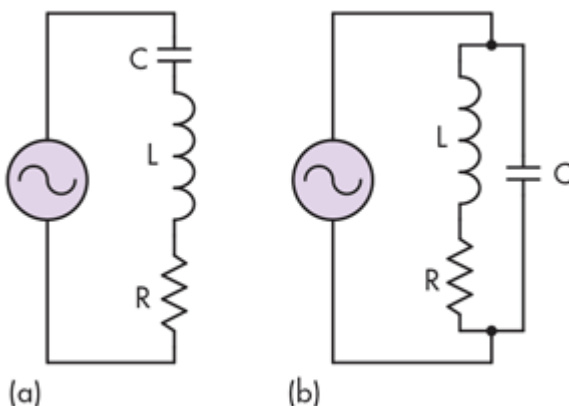
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Classic Resonant Tanks

Figure 1 shows the series and parallel LC tanks. The series LC resonant tank features low impedance at resonance. The coil impedance cancels the capacitor impedance; thus, achieving low impedance enables high current through the LCR circuit. Up to now, the most practical and efficient way to drive high current through a magnetic coil is to use a series resonant circuit.¹ No doubt, then, that the series resonant technique is often used for a high-frequency magnetic field generator.

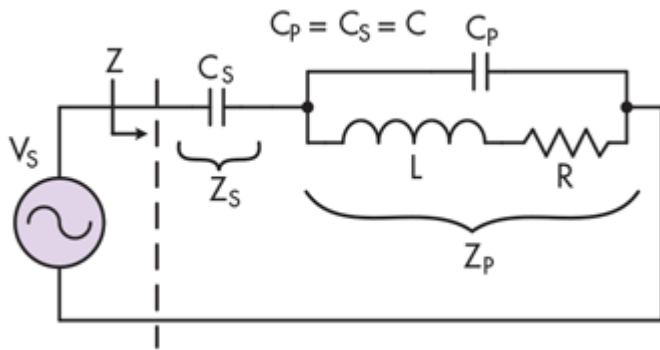


On the other hand, the parallel resonant LC tank's impedance is maximized at resonance. At resonance, the current resonates between the coil and capacitor. The current passing through the magnetic coil is very high while the source current is very low; hence, high impedance. Consequently, the parallel resonant circuit amplifies the source current at resonance. The coil current is generally small in parallel resonance, even with the current amplification effect.

Current-Amplified Resonant

The new current-amplified resonant circuit features low impedance at resonance and current amplification in the magnetic coil (*Fig. 2*). This resonant tank is a

verful, high-frequency, magnetic-field generator. As will be discussed later, current amplification is two es the source or generator current. In addition, the current-amplified resonant circuit is an impedance transformer—at resonance, it transforms the resistance by a factor of four. Therefore, it increases the coil resistance by 4.



Resonant Conditions

The condition for resonance is when the imaginary portion of the impedance, Z , is zero.

$$\text{Img}(Z) = 0 \quad (1)$$

$$\text{Img}(Z_p) + \text{Img}(Z_s) = 0 \quad (2)$$

The resistance in Figure 2 is parasitic in nature and generally small. It has negligible effect on the resonance frequency. For the purpose of resonance-frequency calculation, R is ignored. As we will discuss later, smaller resistance is better a for high-strength and high-frequency magnetic field. The two capacitors are of equal value ($C_S = C_P = C$). From the Appendix, Equation A3, the imaginary part of a parallel resonant impedance Z_P , is given in Eq. 3. The imaginary part of Z_S is just a simple capacitor reactance:

$$\text{Img}(Z_p) = \frac{1}{\omega C - \frac{1}{\omega L}} \quad (3)$$

$$\text{Img}(Z_s) = \frac{1}{\omega C} \quad (4)$$

Substitute Equations 3 and 4 into Equation 2 and it becomes:

$$\frac{1}{\omega C - \frac{1}{\omega L}} + \frac{1}{\omega C} = 0 \quad (5)$$

Solving for ω , which is the current-amplified resonant frequency ω_o :

$$\frac{1}{\omega C - \frac{1}{\omega L}} = -\frac{1}{\omega C} \quad (6)$$

$$\omega_o = \frac{1}{\sqrt{2LC}} = \frac{1}{\sqrt{2}} \frac{1}{\sqrt{LC}} \quad (7)$$

Recall,

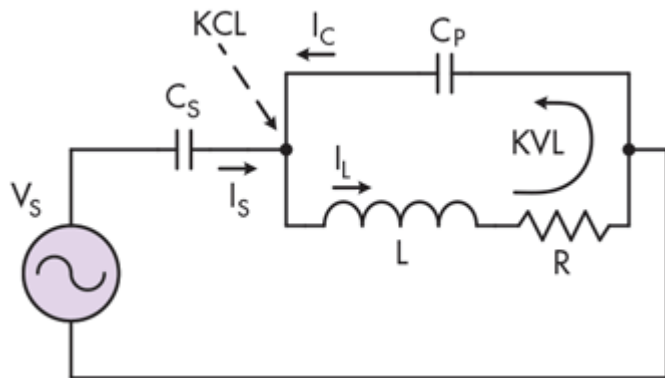
$$f_o = \frac{1}{\sqrt{2}} \left(\frac{1}{2\pi\sqrt{LC}} \right) \quad \omega_o = 1/\sqrt{LC} \text{ is the classic parallel or serial resonant.}$$

From Equation 6 and 7, the new current-amplified resonant

$$\omega C = \frac{1}{\omega L}$$

frequency is $1/\sqrt{2}$ times the classic LC tank resonant frequency. This is because there are two capacitors in the new resonant circuit.

Amplifying Current



The most interesting feature of the new current-amplified resonant circuit is that it amplifies the magnetic-coil current twofold at resonance. That is, the electromagnet current is twice the source generator current. Refer to Figure 3, using the Kirchhoff's voltage law (KVL) around the loop in the parallel tank. Again the small parasitic R is ignored.

$$I_L(j\omega L) + I_C \frac{-j}{\omega C} = 0 \quad (8)$$

Recall from Equation 6 that at resonance, $\omega = 1/\sqrt{2LC}$. Insert Equation 6 into Equation 8.

$$I_L(\omega L) = \frac{I_C}{\omega C}$$

$$I_L = \frac{I_C}{\omega C} \frac{1}{\omega L} = \frac{I_C}{\omega^2 LC}$$

$$I_L = I_C \frac{1}{\left(\frac{1}{\sqrt{2LC}}\right)^2 LC} = 2I_C \quad (9)$$

The magnetic coil current is

twice as much as the capacitor C_P or C_S current (Fig. 3). In fact, the sum of C_P and C_S current is equal to the magnetic-coil current.

Now use Kirchhoff's current law (KCL) to calculate the current at the node where all three currents (I_S , I_C , I_L) are met:

$$I_L = I_S + I_C \quad (10)$$

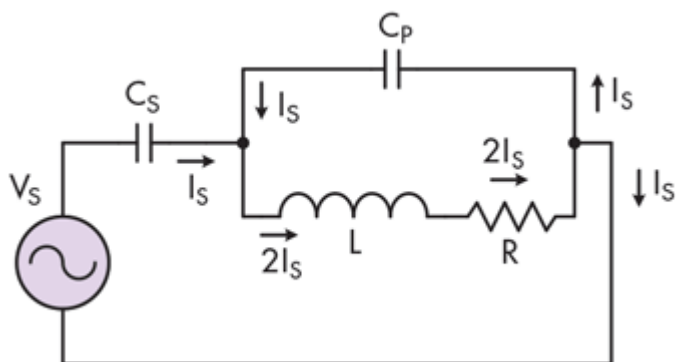
Since I_C is half of I_L :

$$I_L = I_S + \frac{1}{2} I_L \quad (11)$$

$$I_L = 2I_S$$

In summary, the coil current is twice as much as the signal-source generator current. For a given signal generator, the coil current is two times the maximum available current! This is a crucial feature for scientific apparatus that require a high-strength and high-frequency magnetic field. Figure 4 shows the current

flow and how the resonant circuit amplifies current.



Resonant Impedance

As discussed above, at resonance the reactive (imaginary part) impedance is zero. The impedance is real (resistive) at resonance. Since Z_s is reactive only, the real component of Z is coming from Z_p . From Appendix Equation A2, the real part of Z is given as:

$$R_{EQ} = \frac{\frac{R}{(\omega C)^2}}{R^2 + \left(\omega L - \frac{1}{\omega C}\right)^2} \quad (12)$$

Recall that $\omega = 1/\sqrt{2LC}$ at resonance, and substituting it into Equation 12 and simplifying yields:

$$R_{EQ} = \frac{2\frac{RL}{C}}{R^2 + \frac{L}{2C}} \quad (13)$$

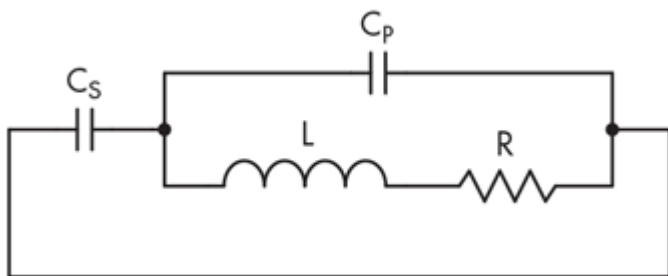
$L/2C$ is much greater than R^2 ; therefore, R^2 is neglected. Thus, Equation 13 is reduced to:

$$R_{EQ} \cong 4R \quad (14)$$

The current-amplified resonant circuit acts like an impedance transformer. It increases the high-frequency coil's resistance by a factor of 4. This new resonant circuit is most advantageous for high-current and low-resistance magnetic coils. It enables high-frequency magnetic-field generation with low source voltage.

Quality-Factor Q

The most important feature of this new current-amplified resonant circuit is its ability to boost current by a factor of 2 for free in order to generate a high-frequency magnetic field. Therefore, the quality factor Q does not impact the current amplification; instead, it affects the resistance. For completeness, Q is discussed here.



The ac voltage source, V_S , is equivalent to a short circuit from the ac signal model's point of view. The current-amplified resonant tank in Figure 2 is redrawn in Figure 5 from the signal model (or energy) point of view. As can be seen, the two capacitors are in parallel and form a single parallel resonant tank. Recall from the classic parallel tank that the Q is equal to:

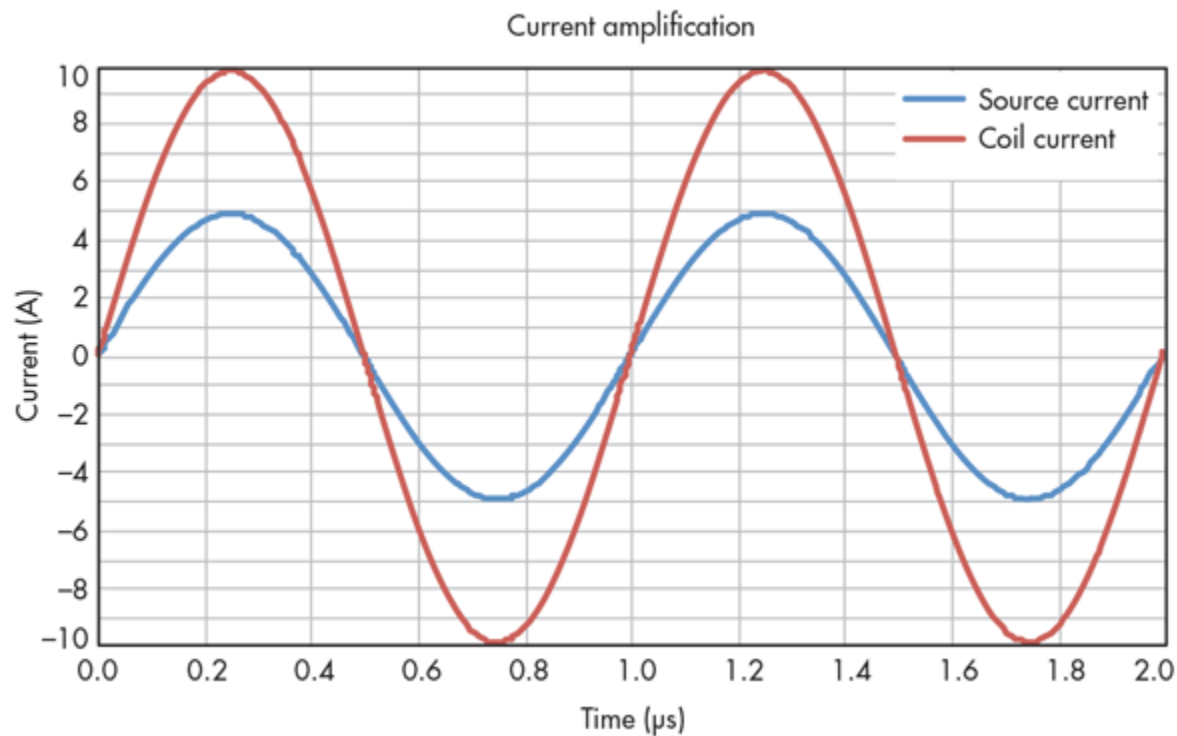
$$Q = \frac{\omega L}{R} \quad (15)$$

Therefore, the Q of the current-amplified resonant tank is the same as the classic parallel resonant tank.

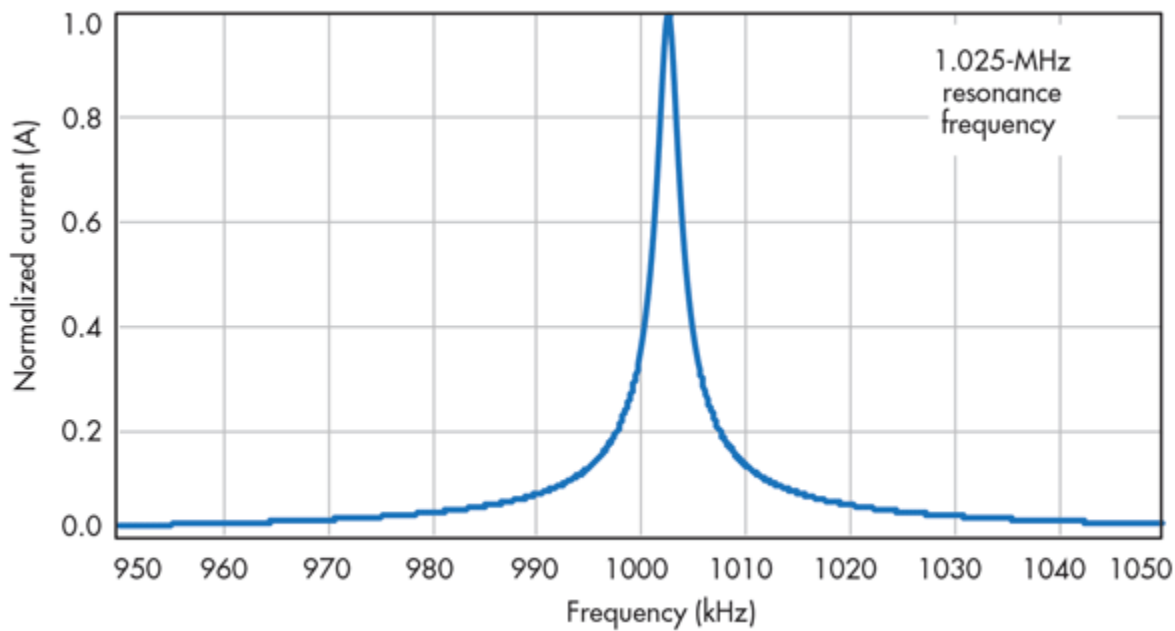
As a confirmation of the previously discussed resonant frequency, the resonant frequency from Figure 5 can be easily found by using the classic parallel tank equation, after taking into account $C_P = C_S = C$:

$$\omega_0 = \frac{1}{\sqrt{L(C_S + C_P)}} = \frac{1}{\sqrt{2LC}} \quad (16)$$

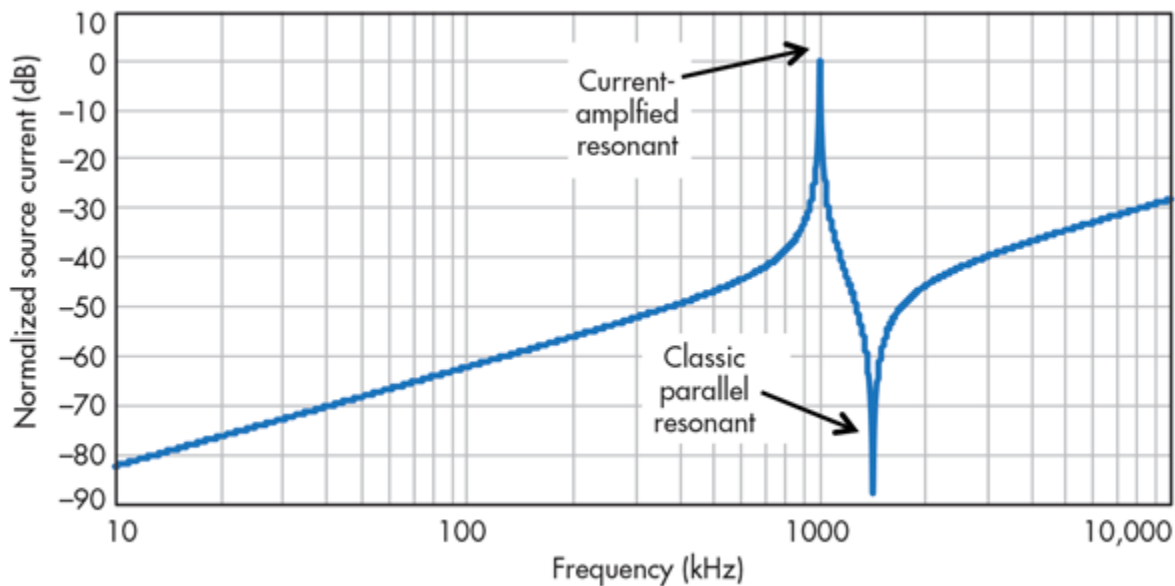
Simulation Results



To confirm the new resonant-circuit mathematical model discussed above, a Spice simulation tool was used to simulate the current-amplified resonant tank in Figure 2. At resonance, the source current is 5 A peak and the coil current is 10 A peak (*Fig. 6*). This confirms the current-amplifying effect of the new resonant tank. Using a 10-μH and two 1.26-nF capacitors, the calculated resonance is 1.0026 MHz. The simulated resonance is 1.025 MHz (*Fig. 7*).

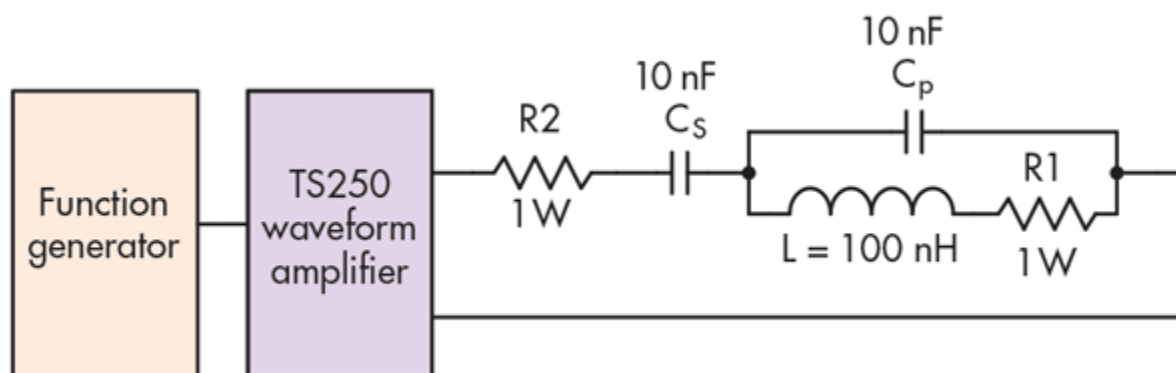


In the simulation, the coil resistance is $125\text{ m}\Omega$, the source voltage is 2.5 V , and the source current is 5 A . This also confirms the tank equivalent impedance is $500\text{ m}\Omega$, as calculated in Equation 14: $4 \times 125\text{ m}\Omega = 500\text{ m}\Omega$. Using the simulation tool, increasing the resistance to $10\text{ }\Omega$ does not change the current amplification factor. Figure 8 plots the source-generator current versus frequency of the current-amplified resonant circuit. It reveals two resonances—the new resonant and the classic parallel resonant. The current-amplified resonant frequency is lower than the classic resonant frequency by a factor of $1/\sqrt{2}$.

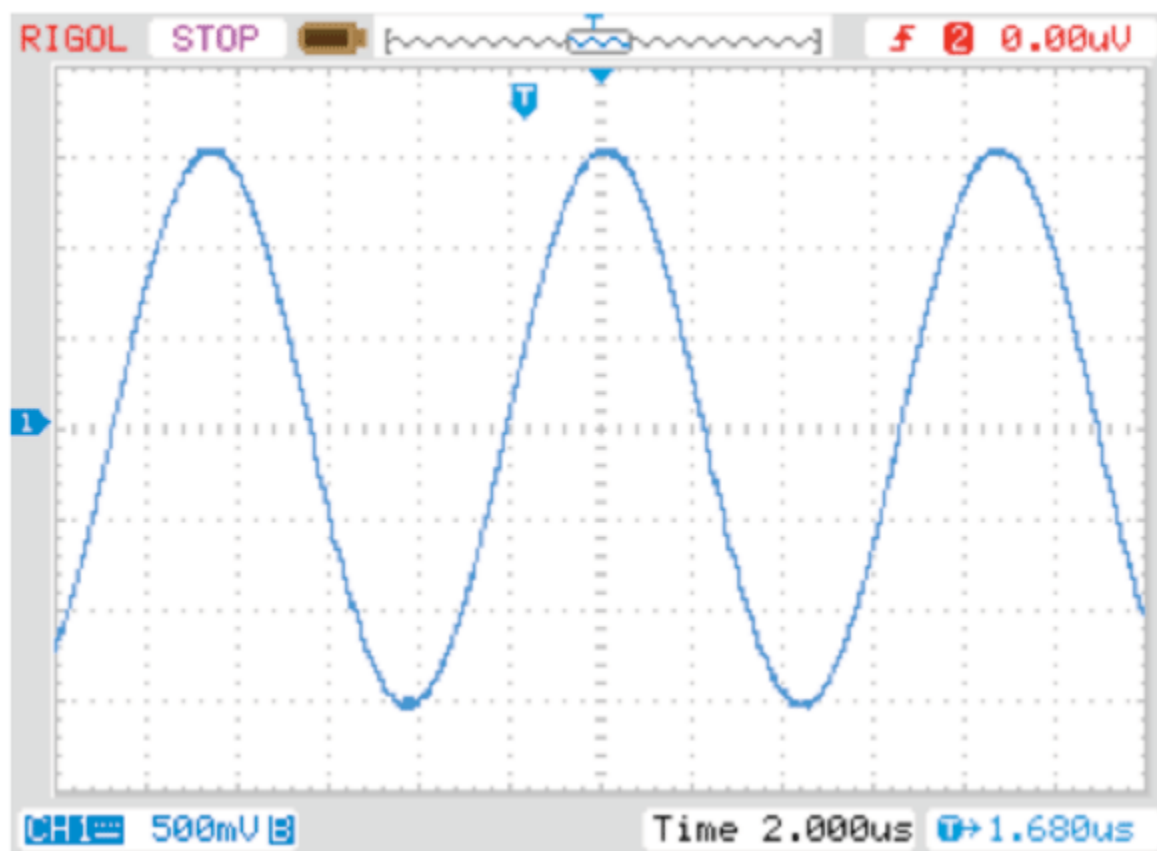


High-Frequency Magnetic-Field Experiment

To verify the magnetic-coil current-amplification effect, a real coil (inductor) was used. The current generator source is the TS250 [high-current function generator amplifier](#)² from [Accel Instruments](#). As shown in Figure 9, the coil is a $100\text{-}\mu\text{H}$ high-current inductor. The two 10-nF capacitors are rated for 1 kV .



A series 1- Ω resistor (R_1) is inserted to monitor the coil current. Another current-sense resistor (R_2) is used to monitor the source current. Measuring current requires measuring the voltage drop across R_1 and R_2 . During the experiment, both 10 m Ω and 100 m Ω have been used for R_1 . For low resistance, the voltage across the sense resistor is so small that the high-frequency magnetic field generated by the coil was interfering with the voltage measurement. Increasing R_1 to 1 Ω showed no sign of interference.



The initial source voltage from the TS250 waveform amplifier was set to 10 V_{P-P} and the initial frequency set to the calculated resonant frequency of 112.5 kHz. Then the frequency was slowly changed until maximum current was observed. This is the 116.5-kHz current-amplified resonant frequency. Subsequently, the voltage amplitude was slowly increased to obtain higher current. At about 30 V_{P-P}, the source current is about 3 A_{P-P} (Fig. 10). As shown in Figure 11, the magnetic coil current was 6 A_{P-P}. As predicted, the coil current is amplified by a factor of 2.



The theoretical current-amplified resonant-circuit impedance is $4\ \Omega$ (not including R_2), which is calculated using Equation 14. The R_1 resistance is amplified by a factor of 4. Adding R_2 resulted in a total theoretical resistance of $\sim 5\ \Omega$. However, the data indicates that 30-V_{P-P} voltage resulted in 3-A_{P-P} , which implies the total impedance is $10\ \Omega$. The magnetic-coil dc resistance is specified at $25\text{ m}\Omega$. It's therefore assumed the coil's ac 116-kHz resistance is much higher due to the skin effect at high frequency. In addition, the capacitors add parasitic resistance. When designing high-frequency magnetic coils for the current-amplified resonant technique, it's important to keep the ac resistance as low as possible.

Conclusion

The novel current-amplified resonant circuit presented here offers a powerful technique for generating high-frequency magnetic fields in scientific and R&D apparatus. The mathematical model predicted the current-amplifying effect in the high-frequency electromagnet. Both simulations and lab experiments confirmed the coil current is amplified by a factor of 2.

References:

1. "[High-Current and High-Frequency Electromagnet Using Resonant Technique](#)," Accel Instruments.
2. "[Waveform Amplifier for Function Generator](#)," Accel Instruments.

Appendix – Parallel Resonant Impedance Derivation

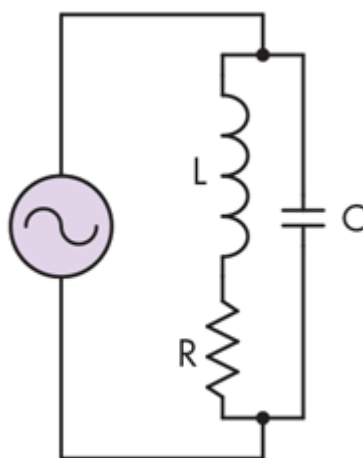


Figure A. The classic parallel resonant circuit consists of RLC to calculate impedance and reactance.

$$Z = \frac{1}{\frac{1}{Z_L} + \frac{1}{Z_C}} = \frac{Z_L Z_C}{Z_L + Z_C} \quad (A1)$$

$$Z_L = R + j\omega L \quad (A2)$$

$$Z_C = \frac{-j}{\omega C}$$

$$Z = \frac{(R + j\omega L) \left(\frac{-j}{\omega C} \right)}{R + j\omega L - \frac{j}{\omega C}}$$

$$Z = \frac{\frac{L}{C} - \frac{jR}{\omega C}}{R + j \left(\omega L - \frac{1}{\omega C} \right)}$$

$$Z = \frac{\frac{L}{C} - \frac{jR}{\omega C}}{R + j \left(\omega L - \frac{1}{\omega C} \right)} \left(\frac{R - j \left(\omega L - \frac{1}{\omega C} \right)}{R - j \left(\omega L - \frac{1}{\omega C} \right)} \right)$$

$$Z = \frac{\frac{RL}{C} - R \left(\frac{L}{C} - \frac{1}{(\omega C)^2} \right) - j \left(\frac{R^2}{\omega C} + \frac{\omega L^2}{C} - \frac{L}{\omega C^2} \right)}{R^2 + \left(\omega L - \frac{1}{\omega C} \right)^2}$$

$$Z = \frac{\frac{R}{(\omega C)^2} - j \left(\frac{R^2}{\omega C} + \frac{\omega L^2}{C} - \frac{L}{\omega C^2} \right)}{R^2 + \left(\omega L - \frac{1}{\omega C} \right)^2}$$

$$\text{Re}(Z) = \frac{R}{R^2 + \left(\omega L - \frac{1}{\omega C} \right)^2}$$

$$\text{Im}(Z)|_{R=0} = \frac{\left(\frac{\omega L^2}{C} - \frac{L}{\omega C^2} \right)}{\left(\omega L - \frac{1}{\omega C} \right)^2} = \frac{\frac{L}{C} \left(\omega L - \frac{1}{\omega C} \right)}{\left(\omega L - \frac{1}{\omega C} \right)^2} = \frac{\frac{L}{C}}{\left(\omega L - \frac{1}{\omega C} \right)} = \frac{1}{\left(\omega C - \frac{1}{\omega L} \right)}$$

(A3)

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